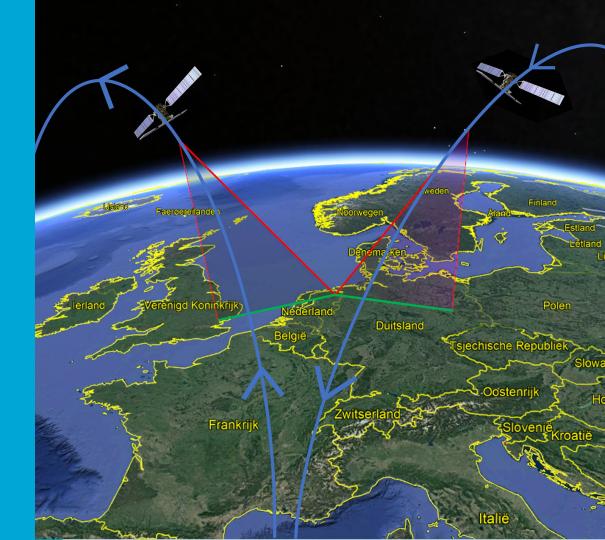
The null line

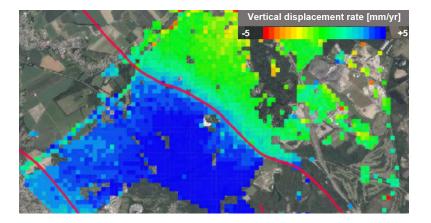
Wietske Brouwer, Andreas Theodosiou, Paco López-Dekker & Ramon Hanssen

LPS - May 24, 2022





Another talk about InSAR geometry?



consecutive interferograms and a stacking approach. For the time series analysis the differential phase of unwrapped interferograms of select consecutive pairs was converted from SAR line-of-sight to vertical displacement using Eq. (1). Vertical displacement is considered to be broadly appropriate for the relatively flat Iqaluit Airport site and is necessary for comparison with thaw tube measurements.

 $d_v = \frac{\varphi(\lambda/4\pi)}{\cos\theta}$

(1)

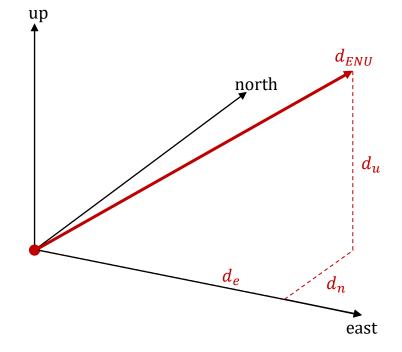
et al., 2001a). Here we first constrain the shape of the magma chamber by reconstructing vertical and horizontal components of the surface displacement using two interferograms, one from an ascending orbit and the other from a descending orbit. This approach is

> Whenever two data sets of InSAR images are available, acquired over the same area and during the same time frame along ascending and descending orbits. the PSInSAR results can be used successfully to estimate the vertical and west–east components of the local displacement field [33]. For the present study, a number



Geometry

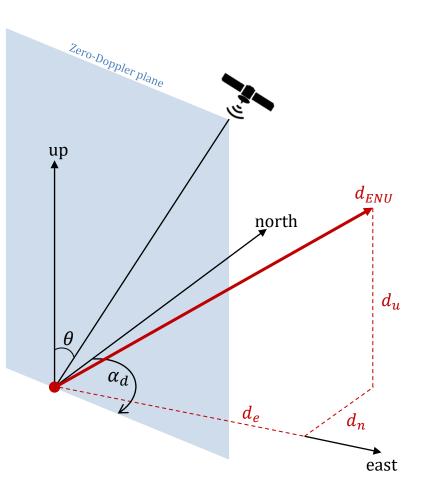
• Displacement vector





Geometry

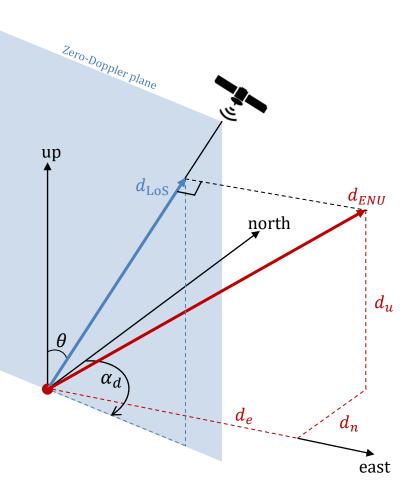
• Displacement vector





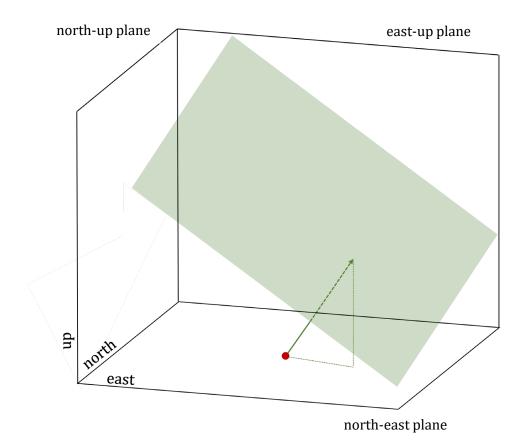
Geometry

- Displacement vector
- LoS observation



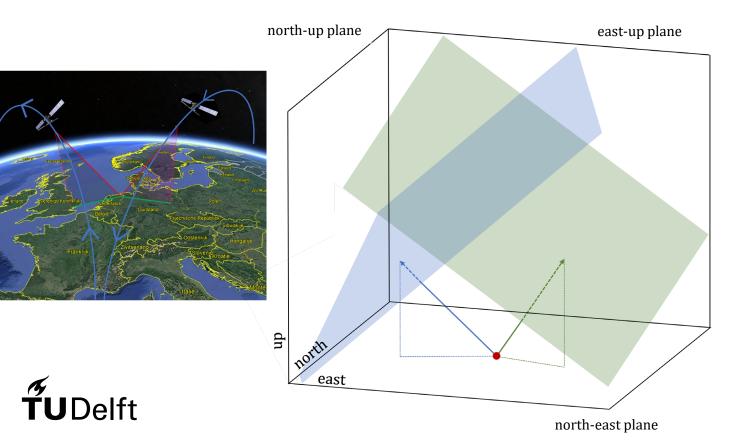


1 LoS observation

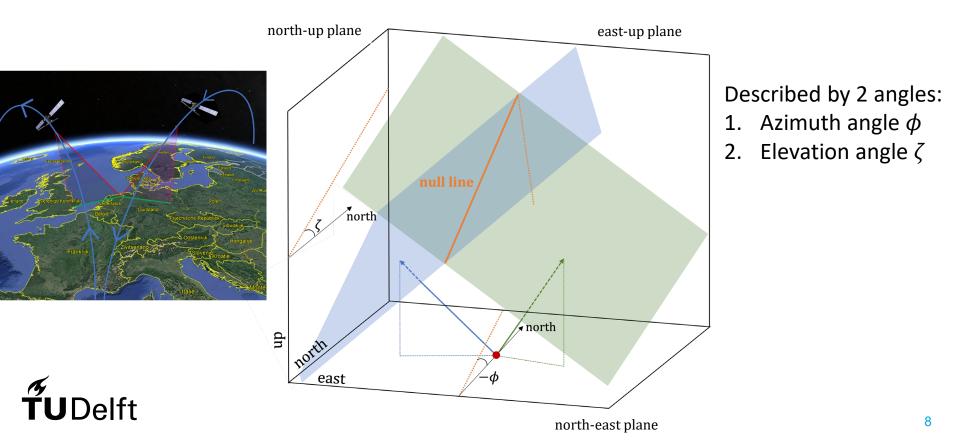




2 LoS observations



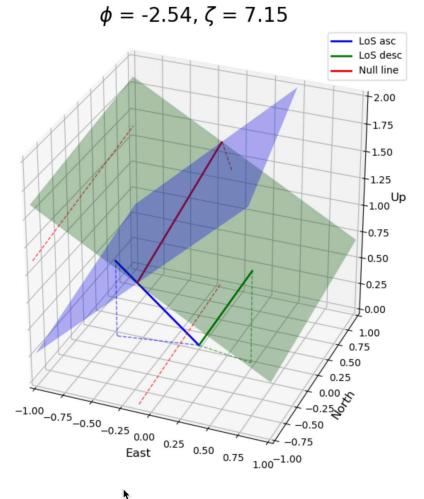
The null line



The null line

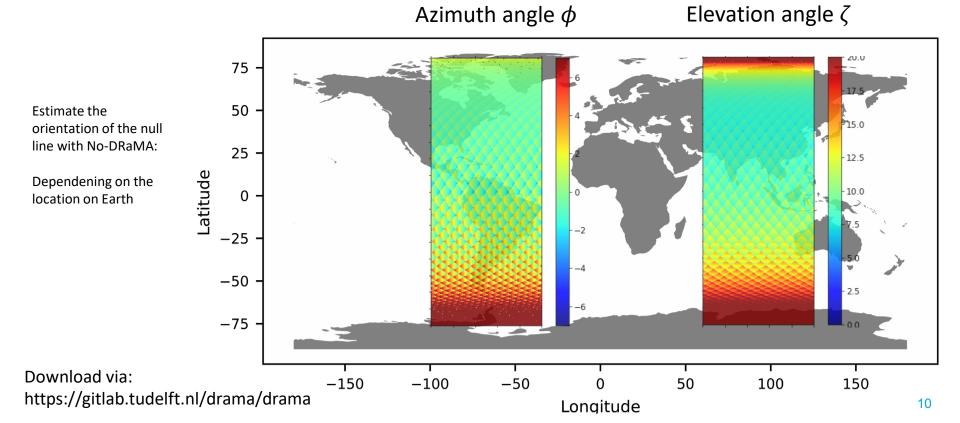
Why?

- 'Blind' for displacements in the direction of the null line
- Adding a third viewing geometry?

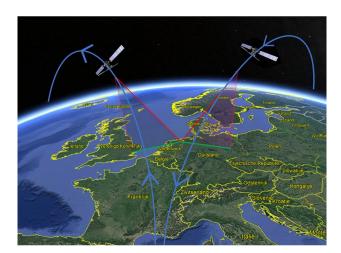




The orientation of the null line: No-DRaMA



east and up \rightarrow Biased estimates



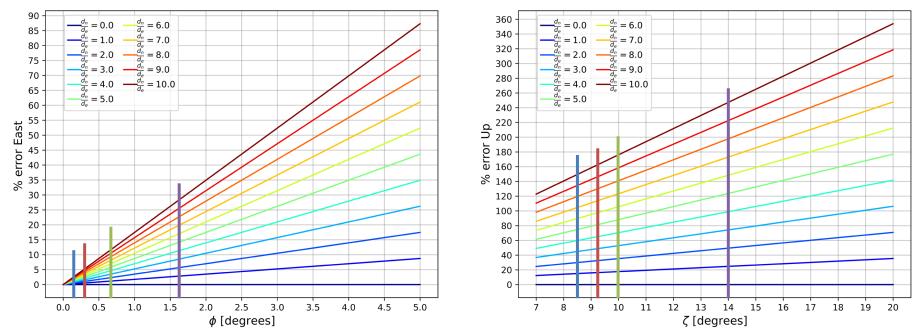
$$E\{\underbrace{\underbrace{d_{\text{LoS}}^{\text{asc}}}_{y}}_{y}\} = \underbrace{\left[\begin{array}{c} \sin(\theta_{1}) \sin(\alpha_{d,1}) & \sin(\theta_{1}) \cos(\alpha_{d,1}) & \cos(\theta_{1}) \\ \sin(\theta_{2}) \sin(\alpha_{d,2}) & \sin(\theta_{2}) \cos(\alpha_{d,2}) & \cos(\theta_{2}) \end{array} \right]}_{A} \underbrace{d_{u}}_{x}$$

$$E\{\underbrace{\underbrace{d_{\text{LoS}}^{\text{asc}}}_{y}}_{y}\} = \underbrace{\left[\begin{array}{c} \sin\theta_{1} \sin\alpha_{d,1} & \cos\theta_{1} \\ \sin\theta_{2} \sin\alpha_{d,2} & \cos\theta_{2} \end{array} \right]}_{A} \underbrace{\left[\begin{array}{c} d_{e} \\ d_{u} \end{bmatrix} \\ x \end{array} \right]}_{x}$$



Biased estimates

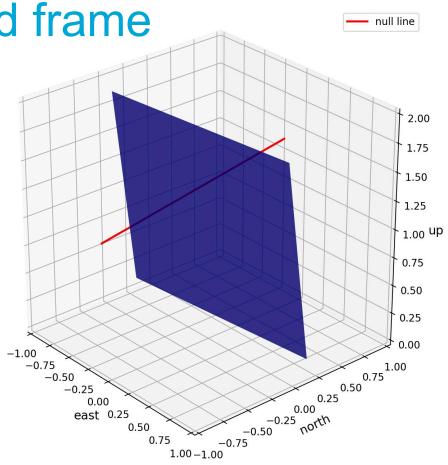
Biased estimates



Bonn: 51° **Los Angeles:** 34° Singapore: 1° Sydney and Cape town: -34°

The null line aligned frame

- Unbiased estimates
- What are going to do with the results?
 - Risk models
 - Finite element models
 - Earth quake models





Conclusions

- Guidelines and taxonomy required
- Always estimate the orientation of the null line
 - No-DRaMA
 - InSAR is blind in the direction of the null line
- Consider to align the reference frame along the null line

