



Optical: Basic Concepts

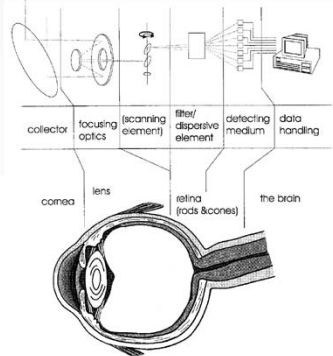
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Lecture D2T1b – 2 July 2013



OPTICAL THEORY – BASIC CONCEPTS

- Radiation laws: definitions and nomenclature
- Sources of radiation in natural environment in the optical domain
- Illumination and observation geometries
- Interaction of radiation with matter in the optical domain
- Radiative transfer in the optical domain
- General solutions for the radiation transfer in the coupled Earth-surface and through the atmosphere
- Derivation of surface reflectance from measured satellite radiances
- Spectral information: signatures of natural objects
- Spatial information: uniformity, textures and scales
- Temporal information: land surface dynamics at multiple scales
- Information retrieval: from spectral indices to model inversion
- Overview of applications

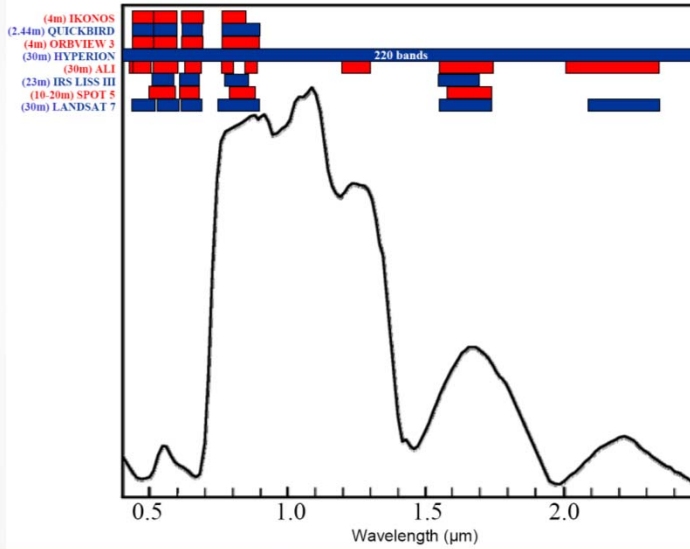


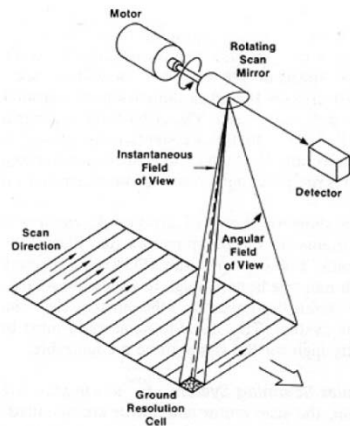
OPTICAL SYSTEMS

Spectral range:
400 - 2500 nm

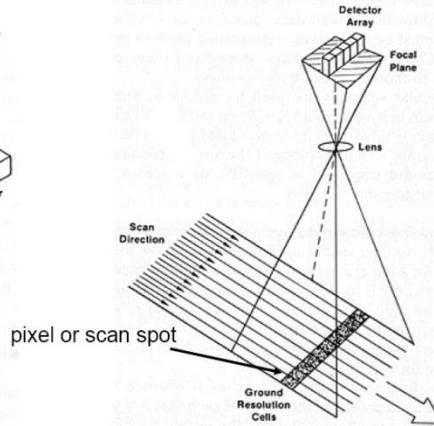
Panchromatic / Broadband:
one single (broad) band (albedo)

Multispectral	Superspectral	Hyperspectral	Ultraspectral
$1 \leq N \leq 10$	$10 \leq N \leq 100$	$100 \leq N \leq 1000$	$1000 \leq N \leq ?$
$\Delta\lambda \approx 100 \text{ nm}$	$\Delta\lambda \approx 50 \text{ nm}$	$\Delta\lambda \approx 10 \text{ nm}$	$\Delta\lambda \approx 1 \text{ nm}$





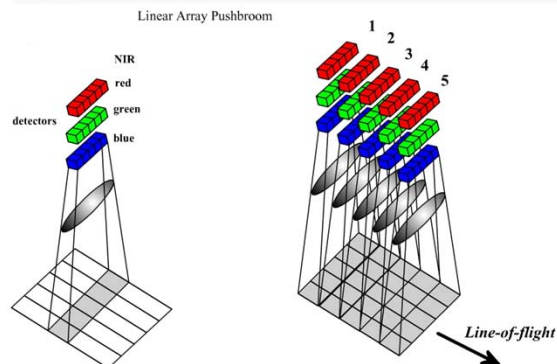
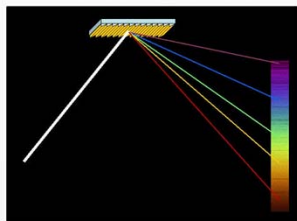
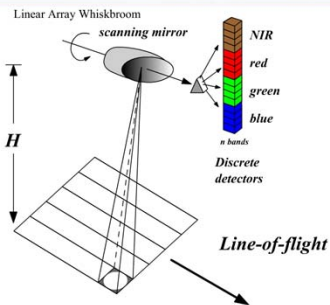
CROSS-TRACK SCANNER.
"Whiskbroom"

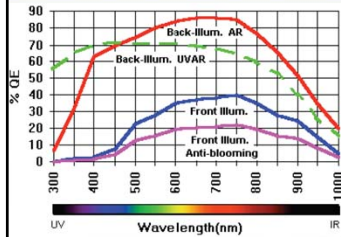


ALONG-TRACK SCANNER.
"Pushbroom"



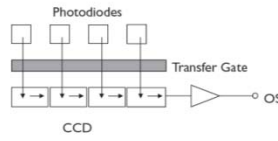
imaging in multiple spectral bands



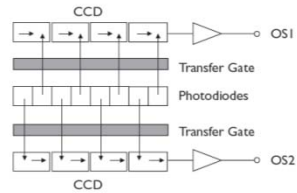


Developments in new sensor technologies

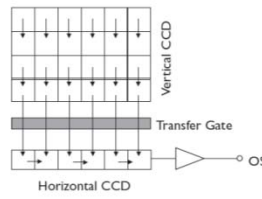
(a) Linear



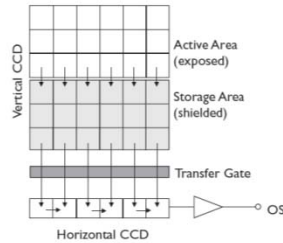
(b) Bi-linear



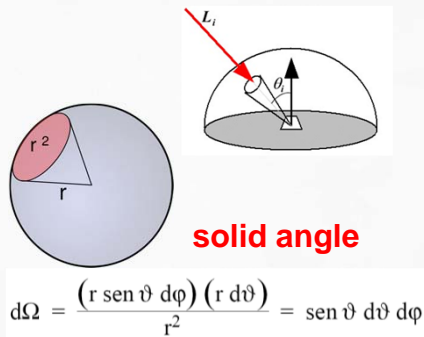
(c) TDI/Area



(d) Frame Transfer



RADIOMETRIC DEFINITIONS

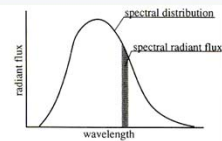


In the particular case of azimuthal symmetry:

$$d\Omega = 2\pi \sin \vartheta d\vartheta$$

Radiant energy Q_e

The energy carried by electromagnetic radiation

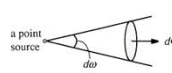


Radiant flux Φ

Radiant energy transmitted per unit time

Radiant intensity I_e

Radiant energy radiated from a point source per solid angle in a radial direction per unit time



Irradiance E_e

Radiant energy incident upon a unit area per unit time



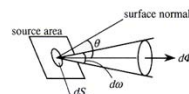
Radiant emittance M_e

Radiant energy radiated from a unit area per unit time



Radiance L_e

Radiant energy radiated from a unit projected area per unit solid angle in a radial direction per unit time



Nomenclature and Radiometric Units

QUANTITY	RADIOMETRIC	Term or quantity	Unit
		Energy content	
FLUX	POWER (WATTS)	radiant energy	joule (J)
FLUX/AREA	IRRADIANCE (WATTS/M²)	energy flow rate	J s ⁻¹ or watt (W)
FLUX/SOLID ANGLE	RADIANT INTENSITY (WATTS/STR)	energy fluence	J m ⁻²
FLUX/AREA/SOLID ANGLE	RADIANCE (WATTS/M²/STR)	energy fluence rate	W m ⁻²
		Photon content	
		number of photons (quanta)	dimensionless
		Avogadro's number of photons	mol
		photon flow rate	s ⁻¹ or mol s ⁻¹
		photon fluence	m ⁻² or mol m ⁻²
		photon fluence rate	m ⁻² s ⁻¹ or mol m ⁻² s ⁻¹

RADIANCE

$$L = \frac{d^2\Phi}{d\Omega dS} = \frac{d^2\Phi}{d\Omega dA \cos\vartheta}$$

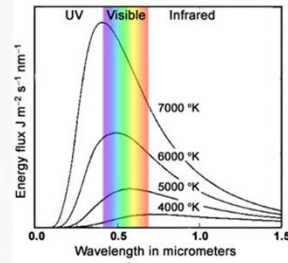
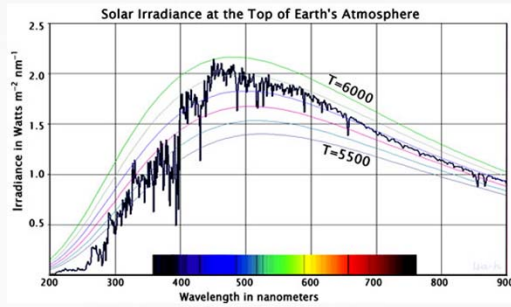
W m⁻² sr⁻¹

$$L = \frac{d^3E}{dt d\Omega dA \cos\vartheta}$$

$$M = \int L \cos\vartheta d\Omega = \int_0^{2\pi} d\varphi \int_0^{\pi/2} d\vartheta L(\vartheta, \varphi) \sin\vartheta \cos\vartheta$$

Lambertian case

$$M = \pi L$$



Planck's Law

$$L_{\lambda}(T) = \frac{2 h c^2}{\lambda^5} \frac{1}{e^{\frac{hc}{\lambda kT}} - 1}$$

$$c = 299792458 \text{ m s}^{-1}$$

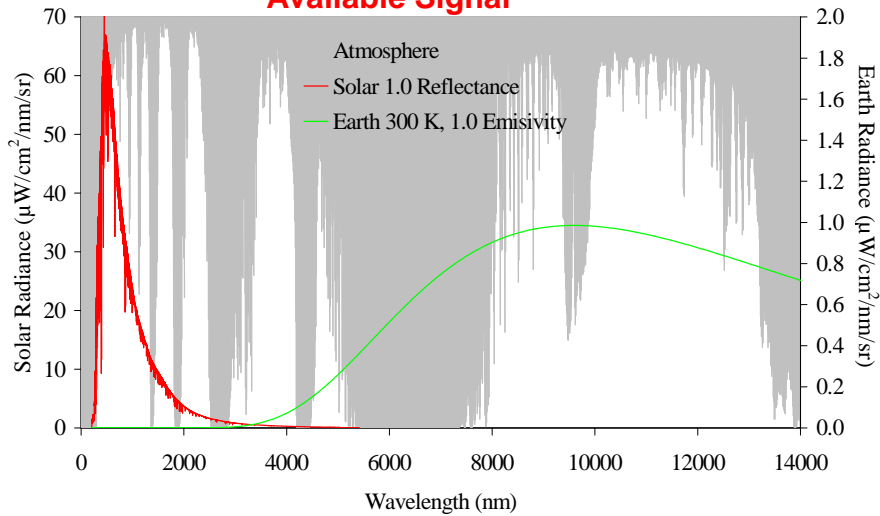
$$h = 6.62606876 \cdot 10^{-34} \text{ J s}$$

$$k = 1.3806503 \cdot 10^{-23} \text{ J K}^{-1}$$

$$\text{W m}^{-2} \text{ sr}^{-1} \mu\text{m}^{-1}$$

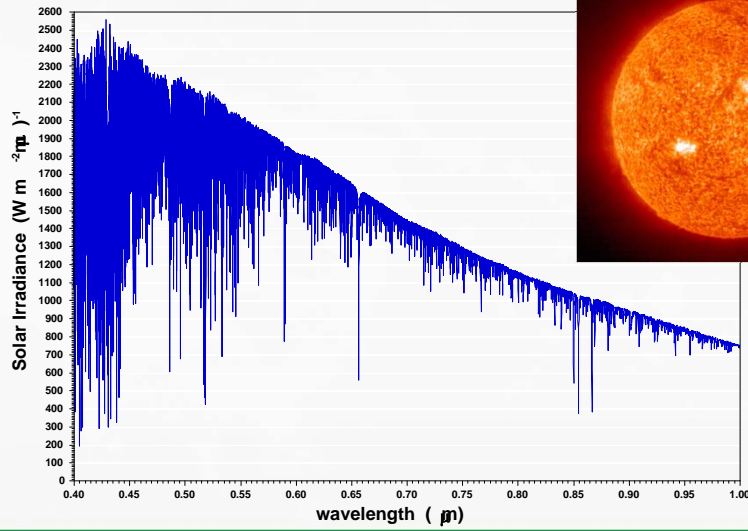


Available Signal

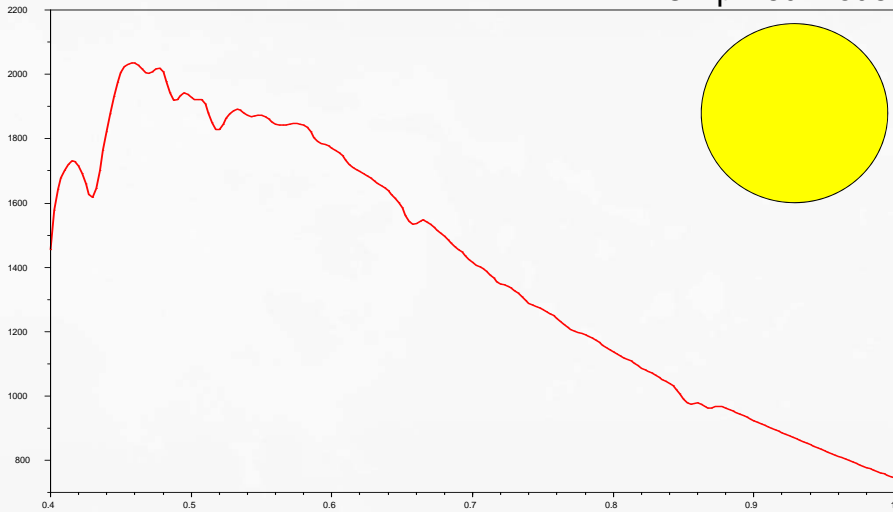




Solar irradiance

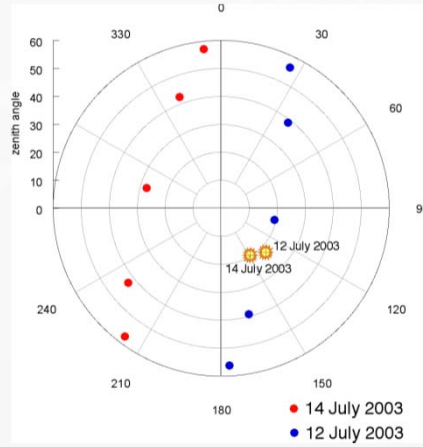
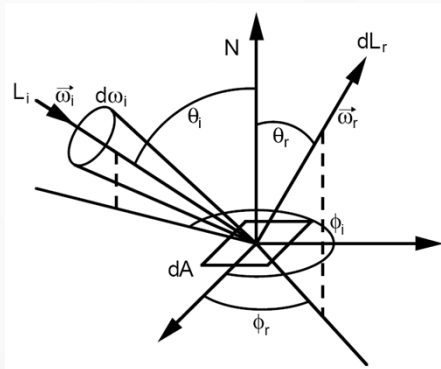


simplified model

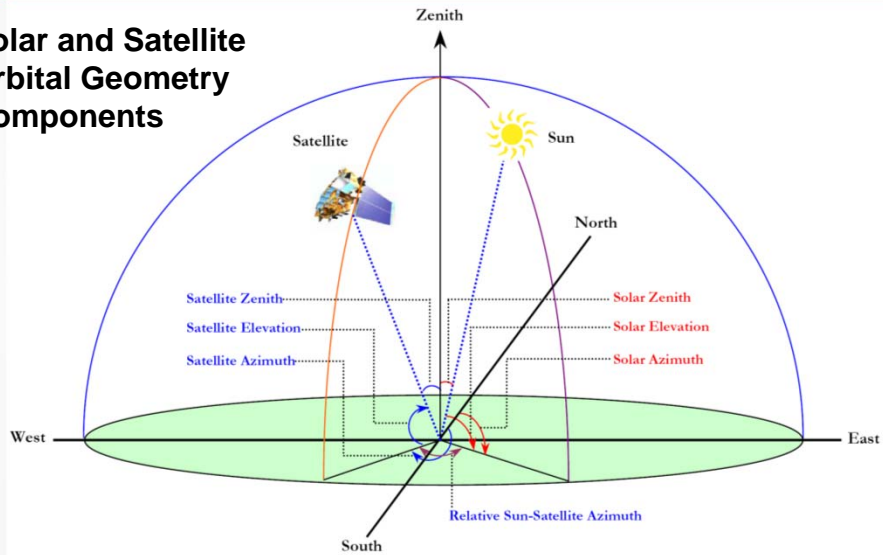


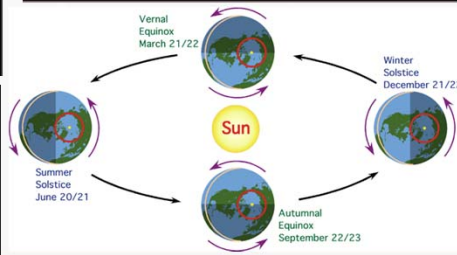
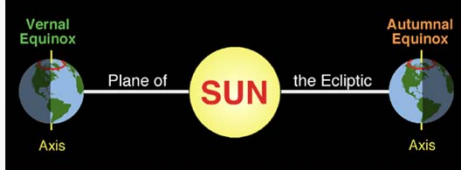
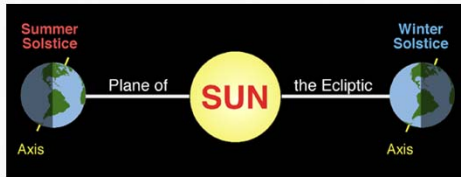
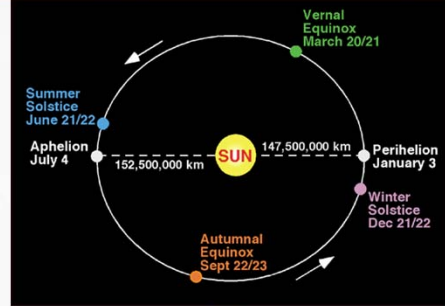
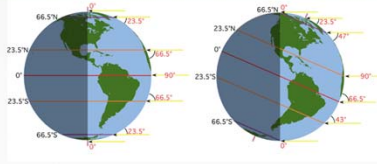


Illumination and observation geometries

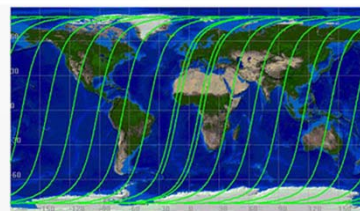
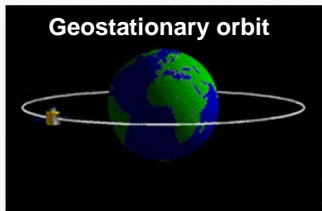
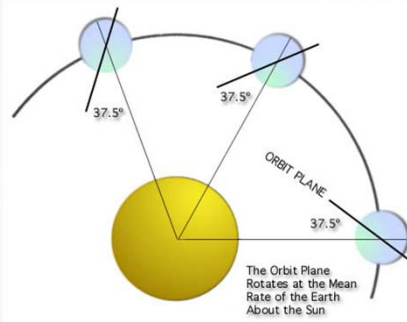
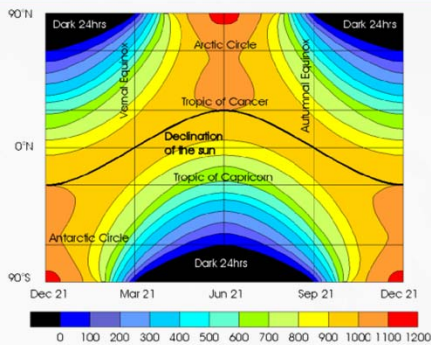


Solar and Satellite Orbital Geometry Components

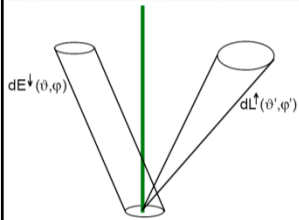




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**Bidirectional Reflectance Distribution Function, BRDF**

$$f(\vartheta, \varphi, \vartheta', \varphi') = \frac{dL^{\uparrow}(\vartheta', \varphi')}{dE^{\downarrow}(\vartheta, \varphi)} \quad \begin{matrix} \text{W m}^{-2} \text{sr}^{-1} \\ \text{W m}^{-2} \end{matrix}$$

$$\text{sr}^{-1}$$

$$f(\vartheta, \varphi, \vartheta', \varphi') = \frac{dL^{\uparrow}(\vartheta', \varphi')}{L^{\downarrow}(\vartheta, \varphi) \cos \vartheta \sin \vartheta \, d\vartheta \, d\varphi} = \frac{dL^{\uparrow}(\vartheta', \varphi')}{L^{\downarrow}(\vartheta, \varphi) \cos \vartheta \, d\Omega}$$

- Very difficult to measure experimentally
- Basic tool in computer graphics

**Conical Reflectance**

$$d\rho(\vartheta, \varphi, \vartheta', \varphi') = \frac{dL^{\uparrow}(\vartheta', \varphi') \cos \vartheta' \, d\Omega'}{L^{\downarrow}(\vartheta, \varphi) \cos \vartheta \, d\Omega} \quad d\rho(\vartheta, \varphi, \vartheta', \varphi') = f(\vartheta, \varphi, \vartheta', \varphi') \cos \vartheta' \, d\Omega'$$

Hemispherical Reflectance

$$\rho = \frac{d\Phi_{\text{hemisf}}^{\uparrow}}{d\Phi_{\text{hemisf}}^{\downarrow}} = \frac{M \, dS}{E \, dS} = \frac{\pi \, L \, dS}{E \, dS} = \frac{\pi \, L}{E}$$

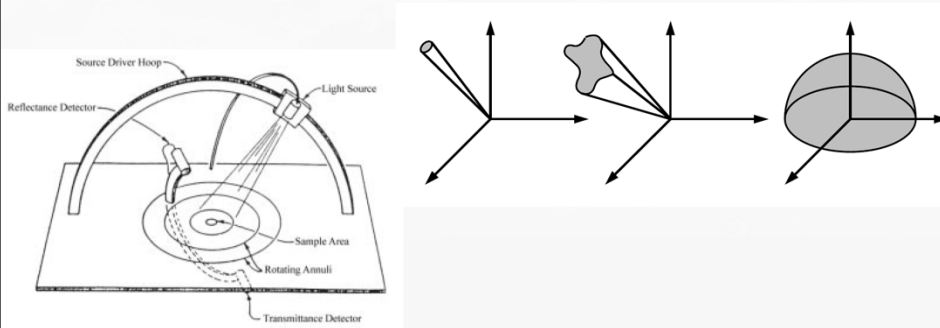
Bidirectional Reflectance Factor

$$R(\vartheta, \varphi, \vartheta', \varphi') = \frac{dL_t^{\uparrow}}{dL_p^{\uparrow}}$$

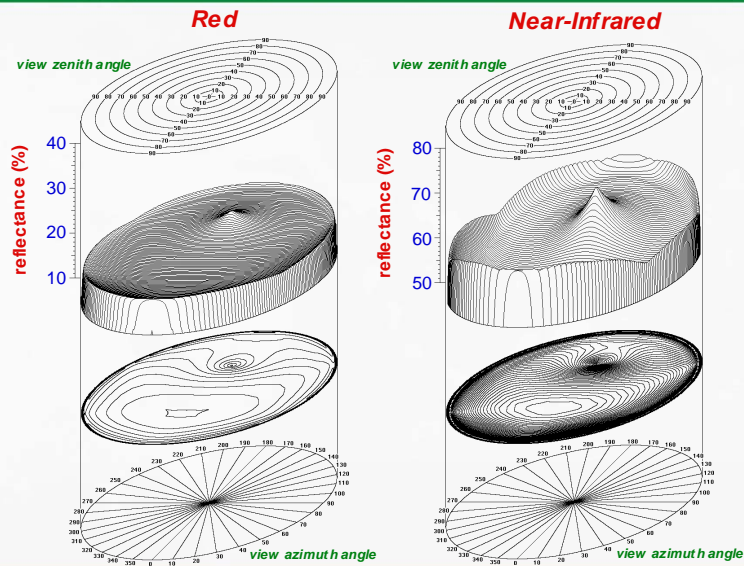


nine types of reflectance measurements

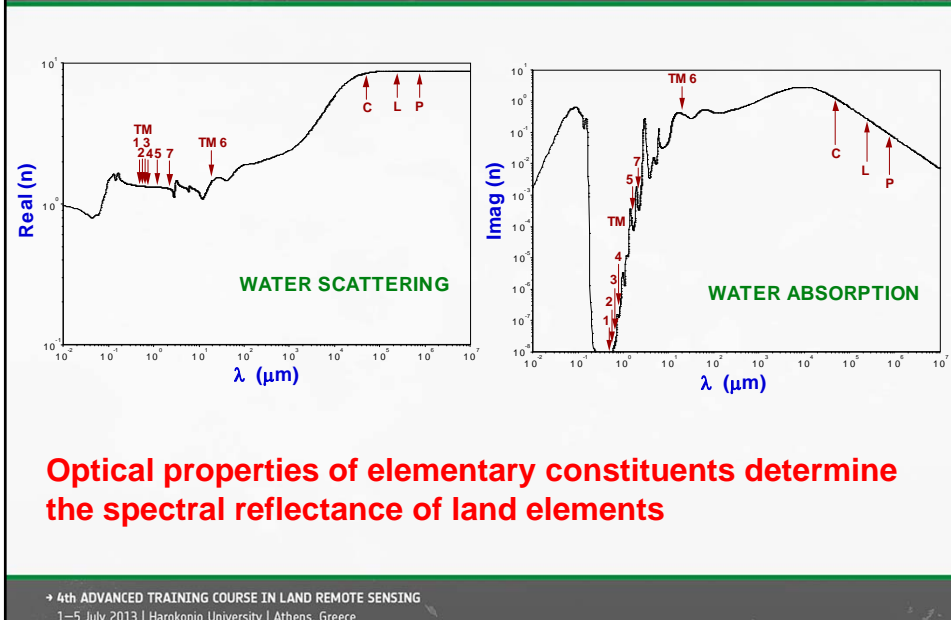
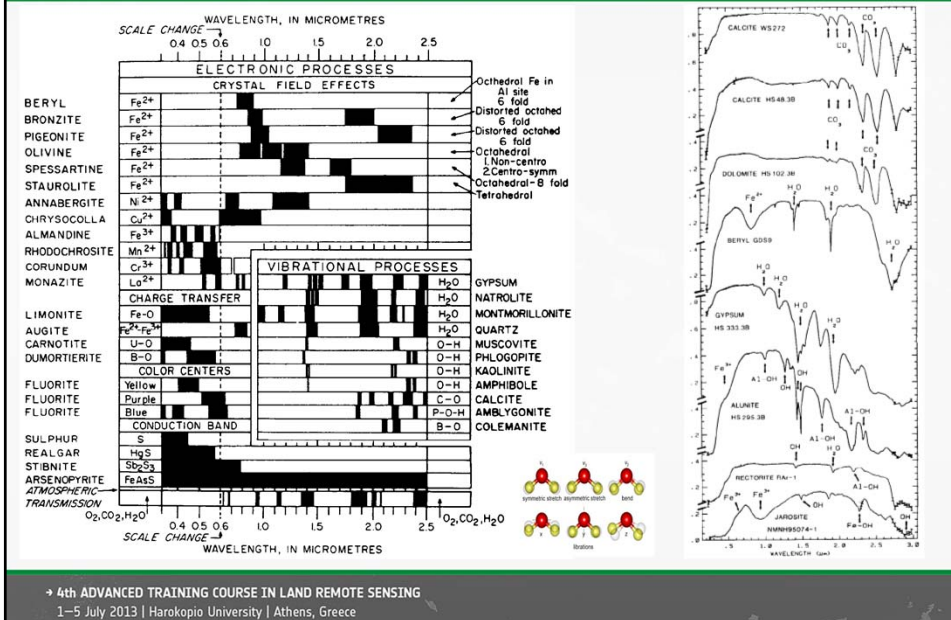
Reflected	Incident		
	directional	conical	hemispherical
directional	bidirectional	conical-directional	hemispherical-directional
conical	directional-conical	biconical	hemispherical-conical
hemispherical	directional-hemispherical	conical-hemispherical	bihemispherical



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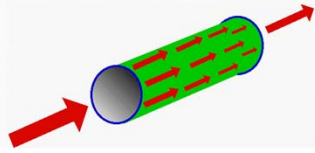
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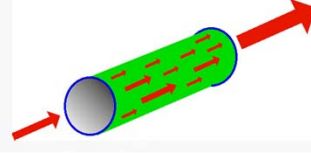


Radiative transfer in the optical domain

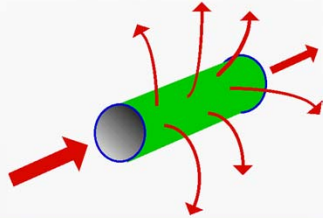
$$- \beta_a^{\text{ext}}(\vec{r}, \vec{\Omega}) \vec{I}(\vec{r}, \vec{\Omega}) dS$$



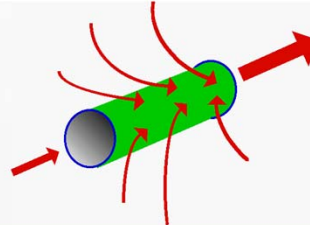
$$+ \beta_a^{\text{int}}(\vec{r}, \vec{\Omega}) \vec{J}_a(\vec{r}, \vec{\Omega}) dS$$



$$- \vec{\beta}_s(\vec{r}, \vec{\Omega}) \cdot \vec{I}(\vec{r}, \vec{\Omega}) dS$$



$$+ \beta_s(\vec{r}, \vec{\Omega}) \vec{J}_s(\vec{r}, \vec{\Omega}) dS$$



General 5D ([3+2]D) vector radiative transfer equation

$$d\vec{I}(\vec{r}, \vec{\Omega}) = - \beta_a^{\text{ext}}(\vec{r}, \vec{\Omega}) \vec{I}(\vec{r}, \vec{\Omega}) dS - \vec{\beta}_s(\vec{r}, \vec{\Omega}) \cdot \vec{I}(\vec{r}, \vec{\Omega}) dS + \\ + \beta_a^{\text{int}}(\vec{r}, \vec{\Omega}) \vec{J}_a(\vec{r}, \vec{\Omega}) dS + \beta_s(\vec{r}, \vec{\Omega}) \vec{J}_s(\vec{r}, \vec{\Omega}) dS$$

$$\vec{J}_s(\vec{r}, \vec{\Omega}) = \frac{1}{4\pi} \int_{4\pi} d\vec{\Omega}' [\hat{\Psi}_s(\vec{r}, \vec{\Omega}, \vec{\Omega}') \cdot \vec{I}(\vec{r}, \vec{\Omega}')]]$$

$$\vec{\beta}_s(\vec{r}, \vec{\Omega}) = \frac{1}{4\pi} \int_{4\pi} d\vec{\Omega}' \hat{\Psi}_s(\vec{r}, \vec{\Omega}, \vec{\Omega}')$$

... this is most times
too complex to be used
in practice...



$$\frac{\partial}{\partial s} \equiv (\vec{\Omega} \cdot \vec{\nabla})$$

$$\frac{1}{\beta_e(\vec{r}, \vec{\Omega})} \frac{\partial}{\partial s} \vec{I}(\vec{r}, \vec{\Omega}) = -\vec{I}(\vec{r}, \vec{\Omega}) + \frac{\omega_0(\vec{r}, \vec{\Omega})}{4\pi} \int_{4\pi} d\vec{\Omega}' [\vec{P}(\vec{r}, \vec{\Omega}, \vec{\Omega}') \cdot \vec{I}(\vec{r}, \vec{\Omega}')] + \vec{J}(\vec{r}, \vec{\Omega})$$

$$d\tau \equiv -\beta_e(\vec{r}, \vec{\Omega}) dz$$

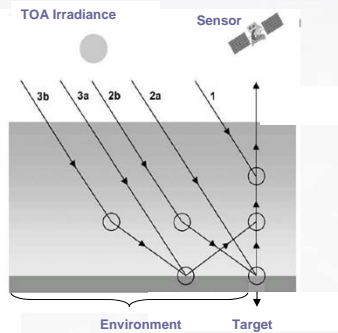
$$d\tau = -\beta_e(\vec{r}, \vec{\Omega}) \cos \vartheta ds$$

$$ds = \frac{dz}{\cos \vartheta}$$



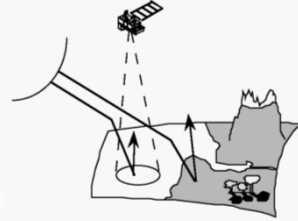
Signal modelling by multiple contributions

$$\begin{aligned} \rho_{\text{sat}} = & \rho_{\text{atm}} + \\ & + T^{\downarrow} \rho_s T^{\uparrow} + \\ & + T^{\downarrow} \rho_s S \rho_s T^{\uparrow} + \\ & + T^{\downarrow} \rho_s S \rho_s S \rho_s T^{\uparrow} + \\ & + T^{\downarrow} \rho_s S \rho_s S \rho_s S \rho_s T^{\uparrow} + \\ & + T^{\downarrow} \rho_s S \rho_s S \rho_s S \rho_s S \rho_s T^{\uparrow} + \\ & + \dots \end{aligned}$$





$$\begin{aligned} \rho_{\text{sat}} &= \rho_{\text{atm}} + \\ &+ T^{\downarrow} \rho_s T^{\uparrow} + \\ &+ T^{\downarrow} (\rho_s)^2 S T^{\uparrow} + \\ &+ T^{\downarrow} (\rho_s)^3 S^2 T^{\uparrow} + \\ &+ T^{\downarrow} (\rho_s)^4 S^3 T^{\uparrow} + \\ &+ T^{\downarrow} (\rho_s)^5 S^4 T^{\uparrow} + \\ &+ \dots = \end{aligned}$$



$$= \rho_{\text{atm}} + T^{\downarrow} [\rho_s + S (\rho_s)^2 + S^2 (\rho_s)^3 + S^3 (\rho_s)^4 + S^4 (\rho_s)^5 + \dots] T^{\uparrow} =$$

$$= \rho_{\text{atm}} + T^{\downarrow} \rho_s [1 + S \rho_s + S^2 (\rho_s)^2 + S^3 (\rho_s)^3 + S^4 (\rho_s)^4 + \dots] T^{\uparrow} =$$

$$= \rho_{\text{atm}} + T^{\downarrow} \rho_s \left[\sum_{n=0}^{\infty} (S \rho_s)^n \right] T^{\uparrow} =$$

$$= \rho_{\text{atm}} + T^{\downarrow} \rho_s \left[\frac{1}{1 - S \rho_s} \right] T^{\uparrow}$$

This approximate solution is very useful in practice !!!



$$\rho_{\text{sat}} = \rho_{\text{atm}} + T_{\text{dir}}^{\downarrow} \check{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dir}}^{\downarrow} \bar{\rho}_s T_{\text{dif}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow}$$

$$\rho_{\text{sat}} = \rho_{\text{atm}} +$$

$$+ T_{\text{dir}}^{\downarrow} \check{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dir}}^{\downarrow} \bar{\rho}_s T_{\text{dif}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} +$$

$$+ T_{\text{dir}}^{\downarrow} \bar{\rho}_s S \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dir}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\rho}_s S \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} +$$

$$+ T_{\text{dir}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s S \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dir}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s S \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} +$$

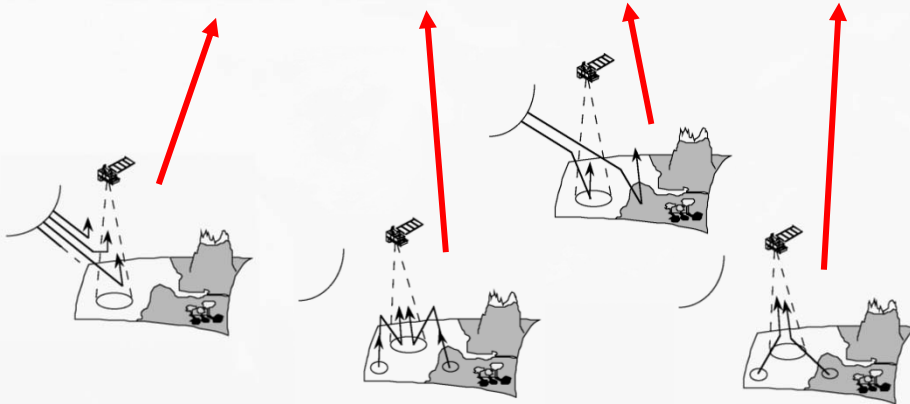
$$+ T_{\text{dir}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s S \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dir}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\rho}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s S \hat{\rho}_s T_{\text{dir}}^{\uparrow} + T_{\text{dif}}^{\downarrow} \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s S \bar{\bar{\rho}}_s T_{\text{dif}}^{\uparrow} +$$

$$+ \dots =$$



SATELLITE SIGNAL MODELLING

$$\rho'(\theta_s, \theta_v, \phi_v) = t_g(\theta_s, \theta_v) \left\{ \rho_a(\theta_s, \theta_v, \phi_v) + \frac{T(\theta_s)}{1 - \langle \rho(M) \rangle_S} [\rho_c(M) e^{-\tau/\mu_v} + \langle \rho(M) \rangle t_d(\theta_v)] \right\}$$



Pre-processing steps:

- Radiometric calibration
- Noise removal
- Cloud screening
- Geometric correction
- Atmospheric correction
- Data integration



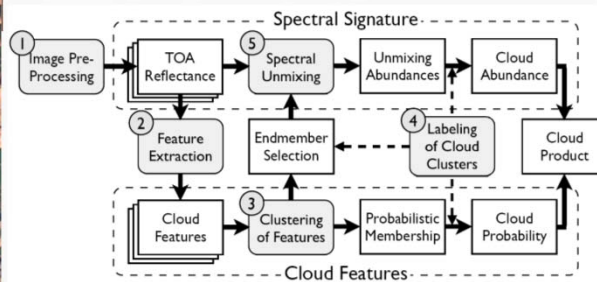
RADIOMETRIC CALIBRATION

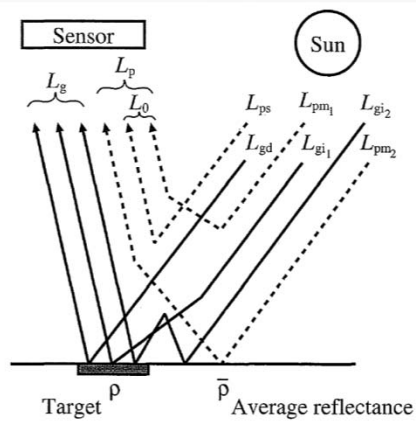
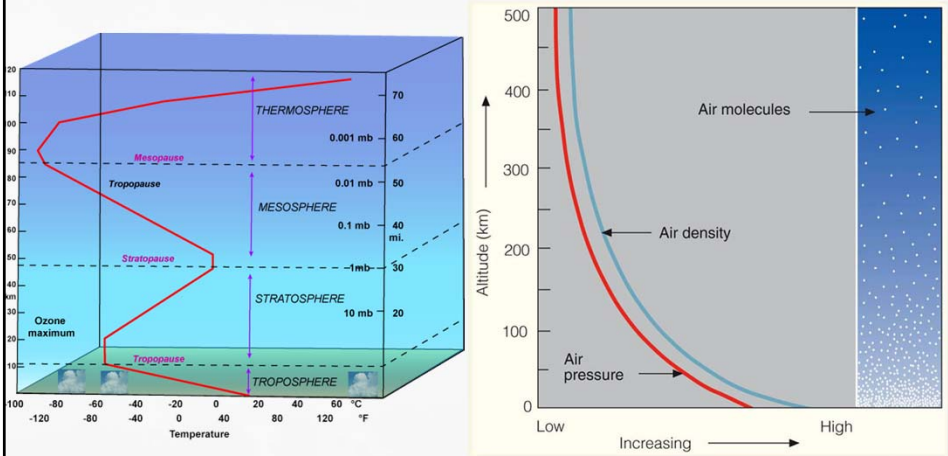
- Pre-launch radiometric calibration to traceable standard (accepted reference)
- Post launch calibration campaigns to maintain/monitoring in flight calibration (vicarious)
- On-board calibration (both radiometric and spectral)



CLOUD SCREENING

- Very dependent on the available spectral information
- Many different algorithms (from simple thresholds up to sophisticate techniques)





- The atmosphere modifies the radiation measured by optical sensors:
- Aerosols and gases present optical activity at VIS/NIR/SWIR.
- Reflectance increases/decreases depending on the wavelength.
- Image loses contrast.

→ Removing the atmospheric influence from remote sensing data is necessary before the data exploitation



Surface reflectance retrieval

- TOA radiance modeled assuming Lambertian reflectance for the target:

$$L_{\text{TOA}} = L_0 + \frac{1}{\pi} \frac{\rho_s (E_{\text{dir}} \mu_{\text{il}} + E_{\text{dif}}) T_{\uparrow}}{1 - S \rho_s}$$

- Analytically invertible to retrieve ρ_s .

$$\rho_s = \frac{L_{\text{TOA}} - L_0}{[(E_{\text{dir}} \mu_{\text{il}} + E_{\text{dif}}) \frac{T_{\uparrow}}{\pi}] + S[L_{\text{TOA}} - L_0]}$$

- Removal of adjacency effects



INVERSION OF SURFACE REFLECTANCE

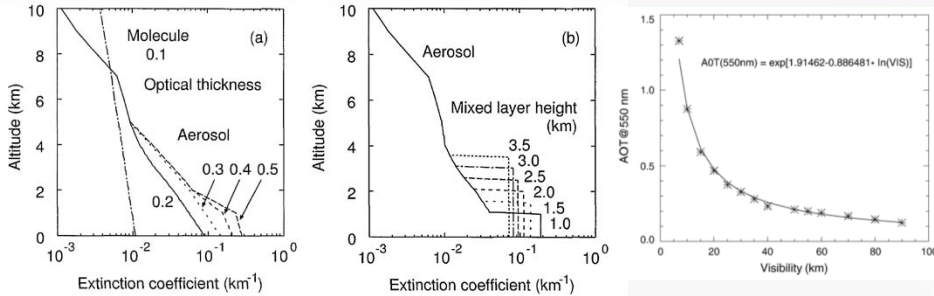
Flat Lambertian areas:

$$\rho' = A + \frac{B \rho_c + C \langle \rho \rangle}{1 - S \langle \rho \rangle}$$

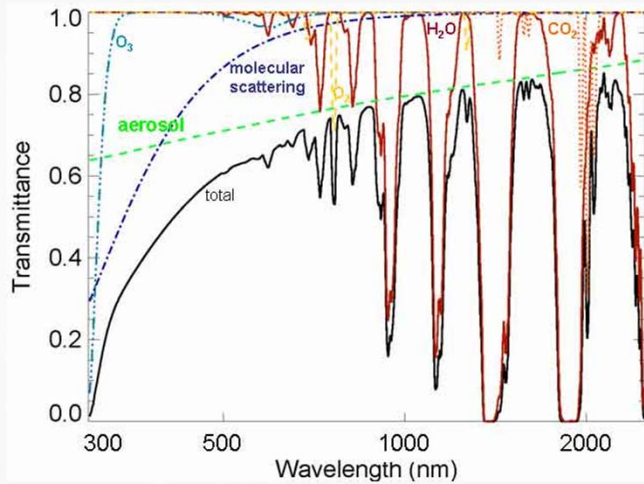
$$\rho_c = \frac{\left(\frac{\rho' - A}{B} \right) - \frac{C}{B+C} \left(\frac{\langle \rho' \rangle - A}{B} \right)}{1 + S \frac{B}{B+C} \left(\frac{\langle \rho' \rangle - A}{B} \right)}$$

Non-Lambertian areas with topographic structure:

- no analytic inversion under approximations
- decoupling 'effective' reflectances and 'effective' geometric terms required for environment
- multistep numerical procedure required for inversion
- multiple reflection terms only significant for high reflectance surroundings



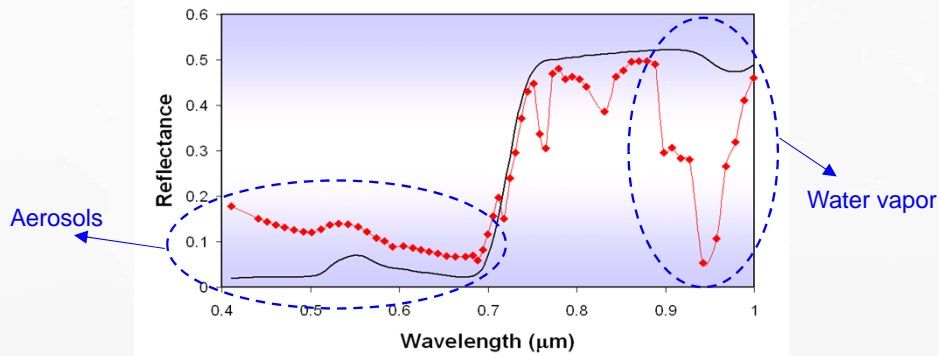
Permanent Constituents		Variable constituents	
Constituent	% by volume	Constituent	% by volume
Nitrogen (N ₂)	78.084	Water Vapor (H ₂ O)	0.04
Oxygen (O ₂)	20.948	Ozone (O ₃)	12 x 10 ⁻⁴
Argon (Ar)	0.934	Sulfur dioxide (SO ₂) ^b	0.001 x 10 ⁻⁴
Carbon dioxide (CO ₂)	0.033	Nitrogen dioxide (NO ₂)	0.001 x 10 ⁻⁴
Neon (Ne)	18.18 x 10 ⁻⁴	Ammonia (NH ₃)	0.001 x 10 ⁻⁴
Helium (He)	5.24 x 10 ⁻⁴	Nitric oxide (NO)	0.0005 x 10 ⁻⁴
Krypton (Kr)	1.14 x 10 ⁻⁴	Hydrogen sulfide (H ₂ S)	0.00005 x 10 ⁻⁴
Xenon (Xe)	0.089 x 10 ⁻⁴	Nitric acid vapor	trace
Hydrogen (H ₂)	0.5 x 10 ⁻⁴		
Methane (CH ₄)	1.5 x 10 ⁻⁴		
Nitrous Oxide (N ₂ O)	0.27 x 10 ⁻⁴		
Carbon Monoxide (CO)	0.19 x 10 ⁻⁴		





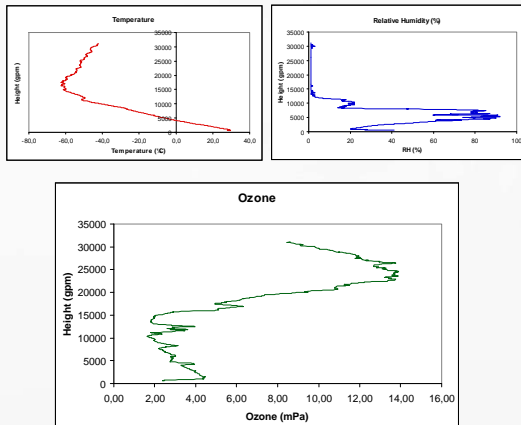
Surface reflectance retrieval

Atmospheric correction: Removal of the atmospheric effects from the measured at-sensor radiance, leading to the derivation of surface reflectance images.

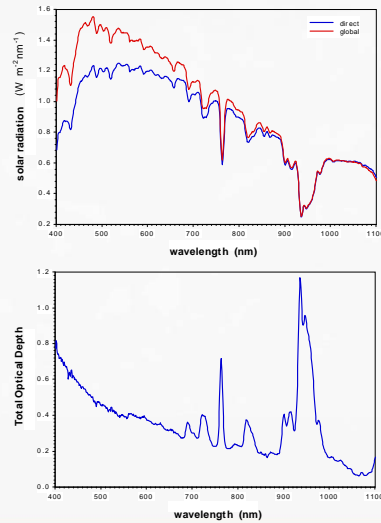


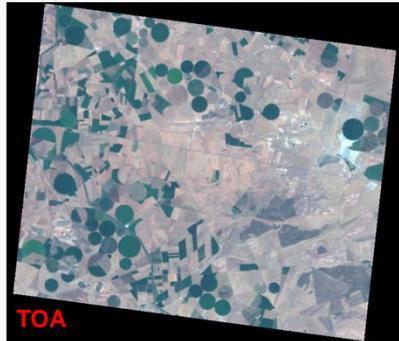
ATMOSPHERIC INFORMATION

In-situ radiosoundings

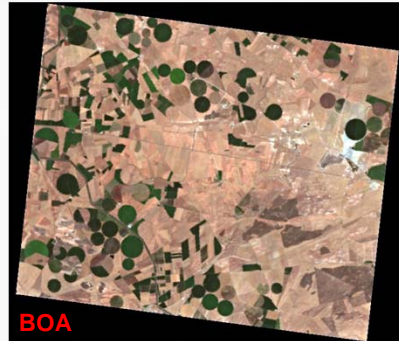


In-situ spectral irradiance





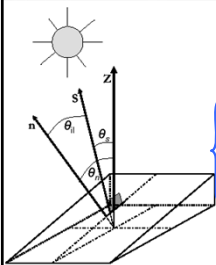
TOA



BOA



Topographic effects



$$L_{TOA} = L_0 + \frac{1}{\pi} \frac{\rho_s (E_{dif} \mu_{il} + E_{dif} T \uparrow)}{1 - S \rho_s}$$

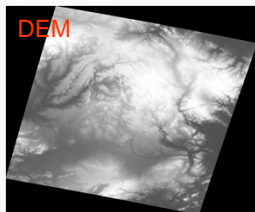
$$\mu_{il} = \mathbf{n} \cdot \mathbf{S} \rightarrow \text{Cosine correction}$$

$$E_{dif}^t(x, y, z) = E_{dif}(z) \left[t_{dir}(z) \mu_{il}(x, y) + [1 - t_{dir}(z) \mu_s] \frac{1 + \mu_n(x, y)}{2} \right]$$

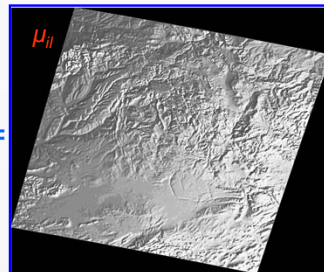
→ Hay's model

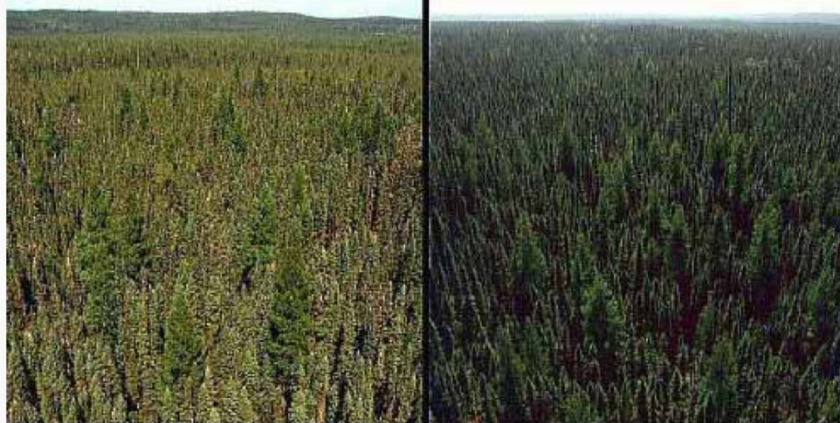


+

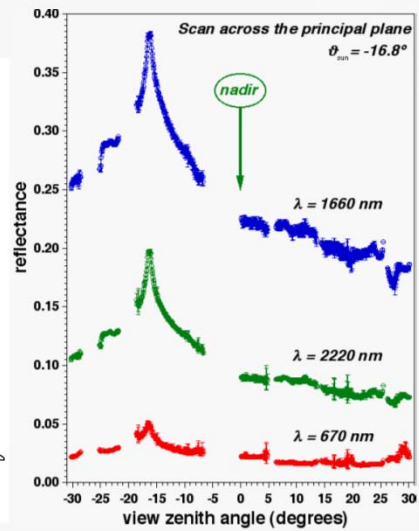
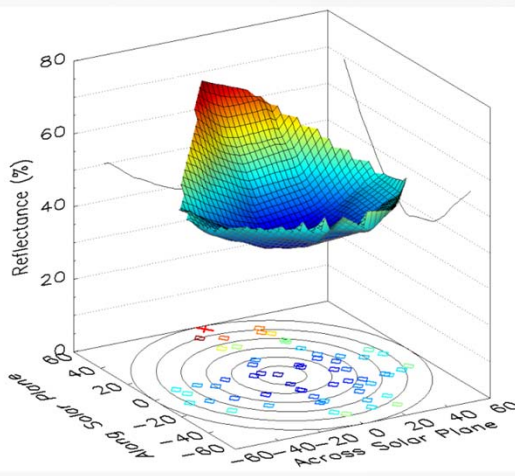


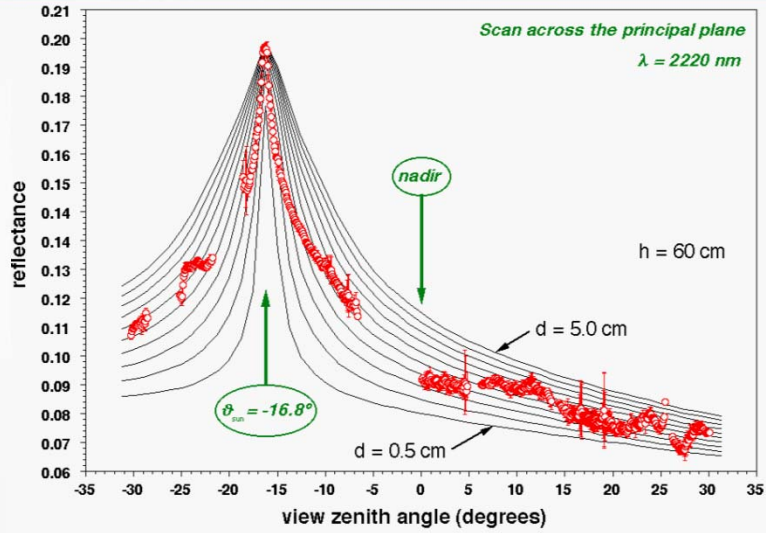
=



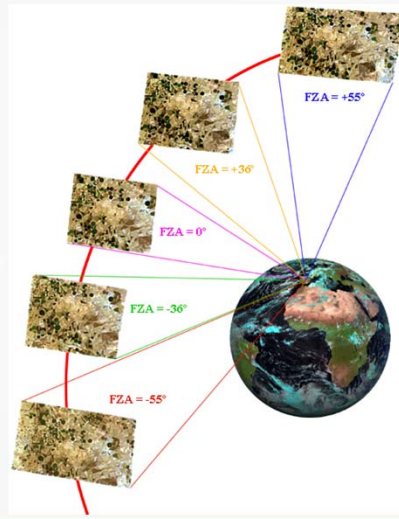
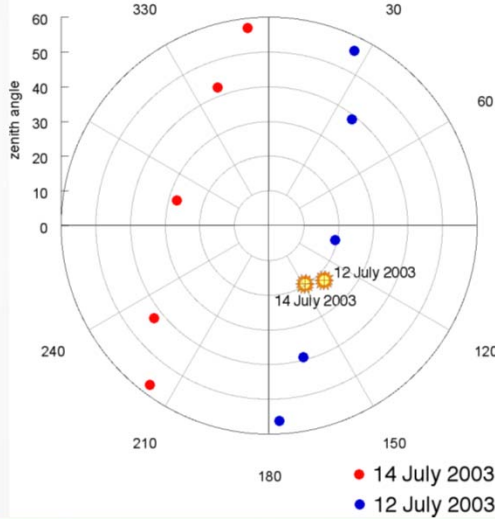


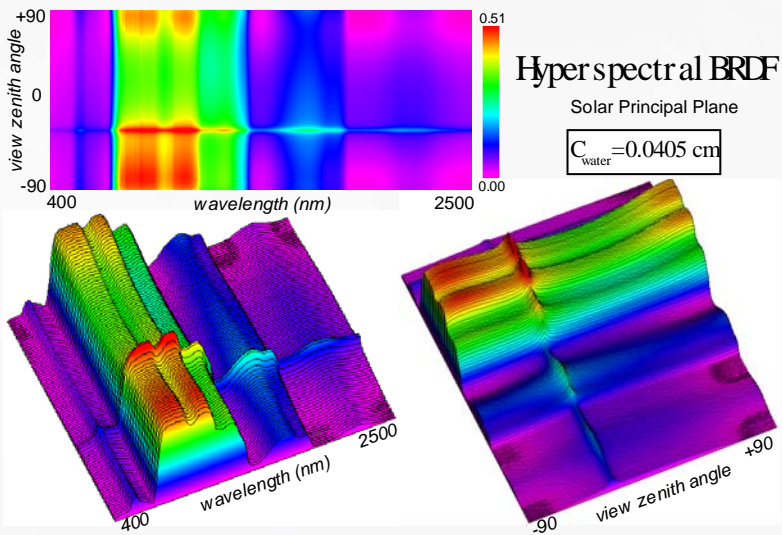
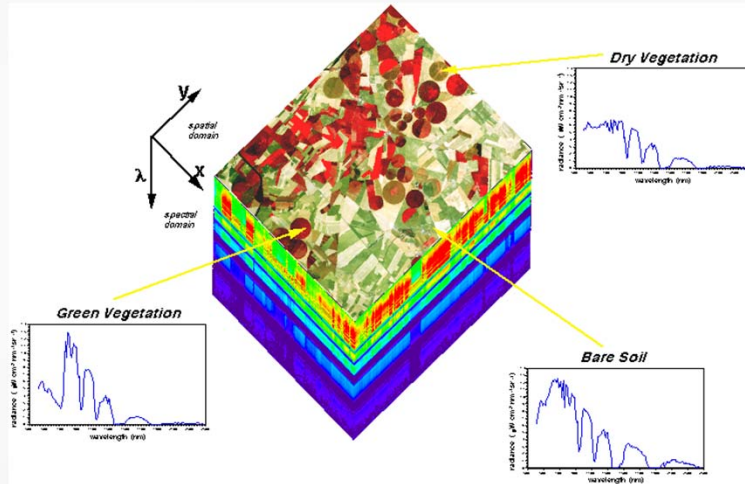
BRDF effects





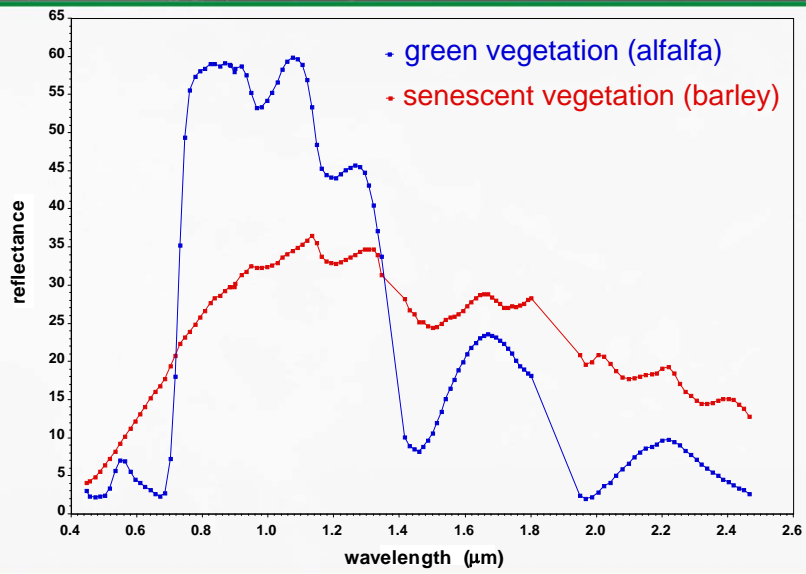
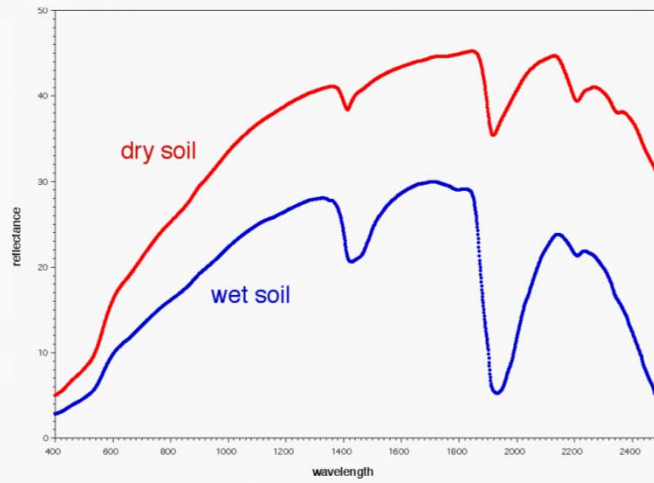
CHRIS/PROBA satellite view angles

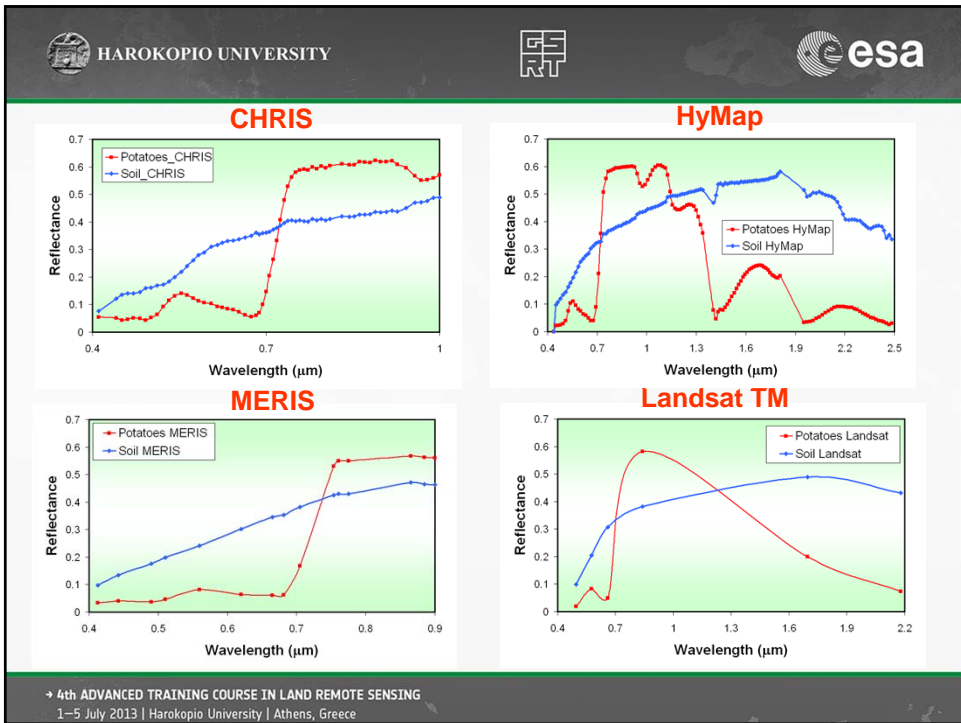
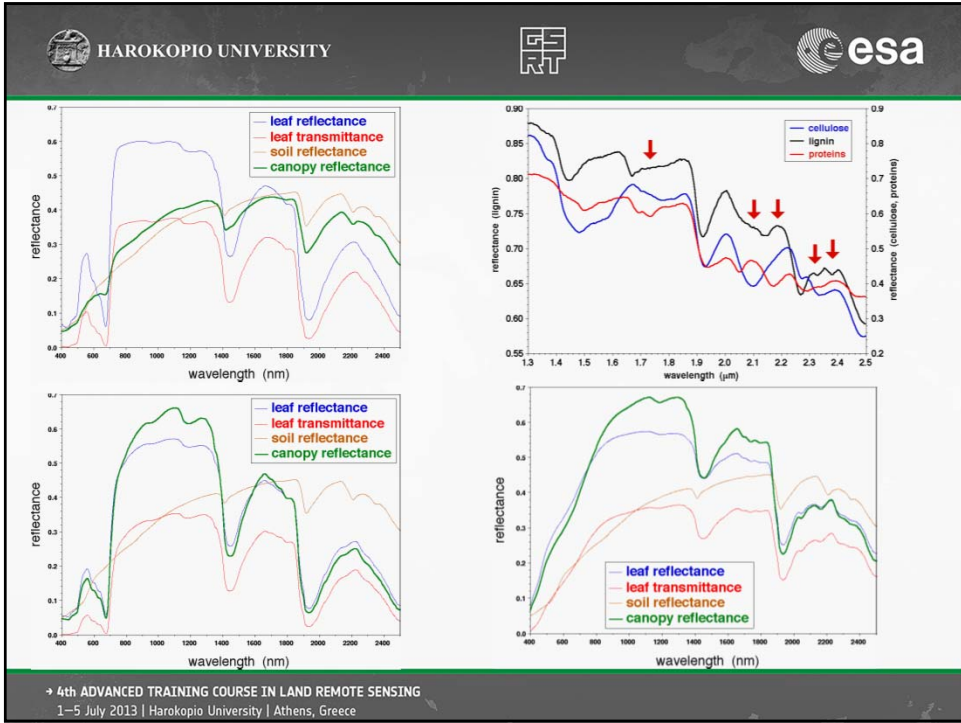


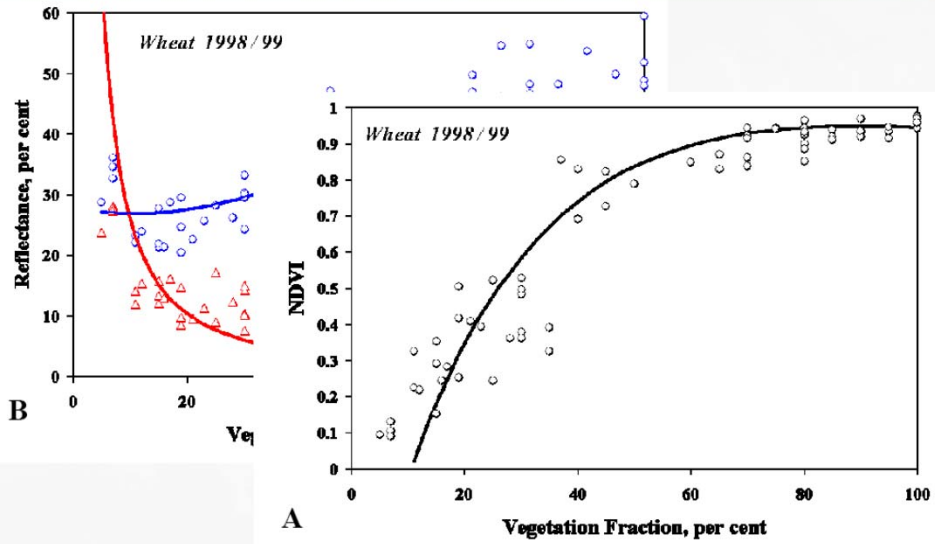




SOIL REFLECTANCE

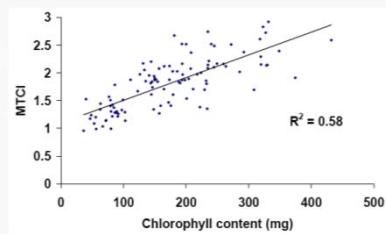
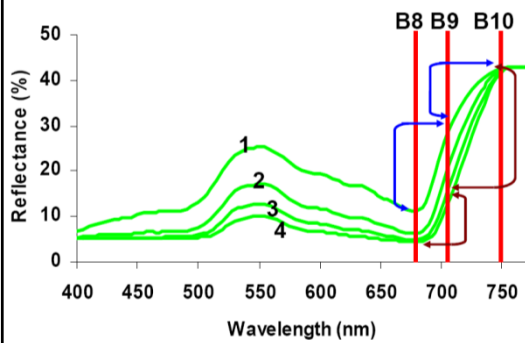


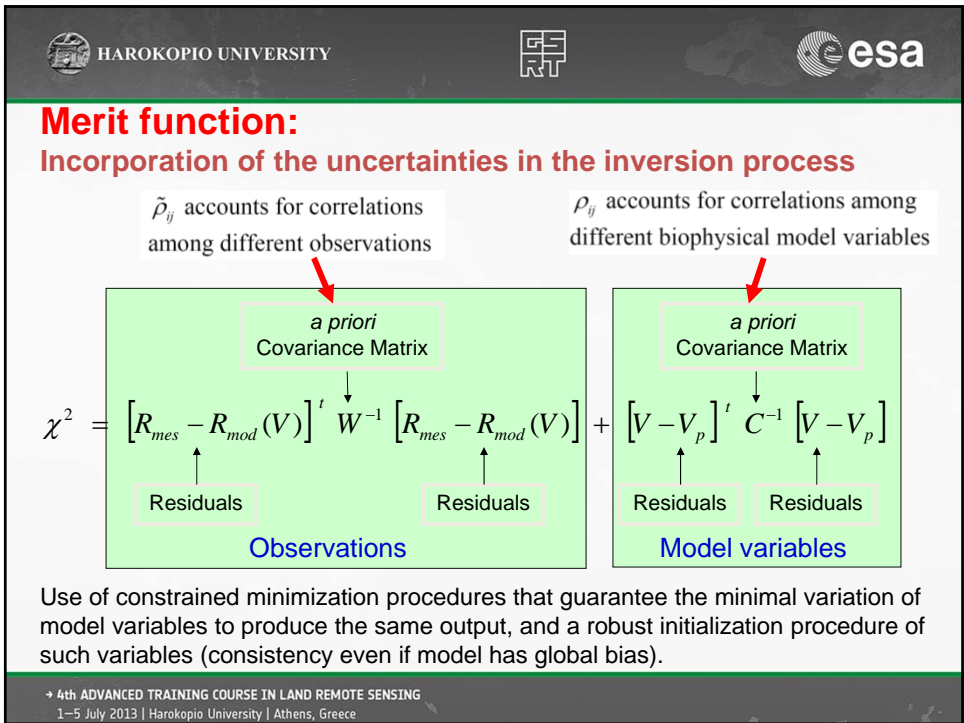
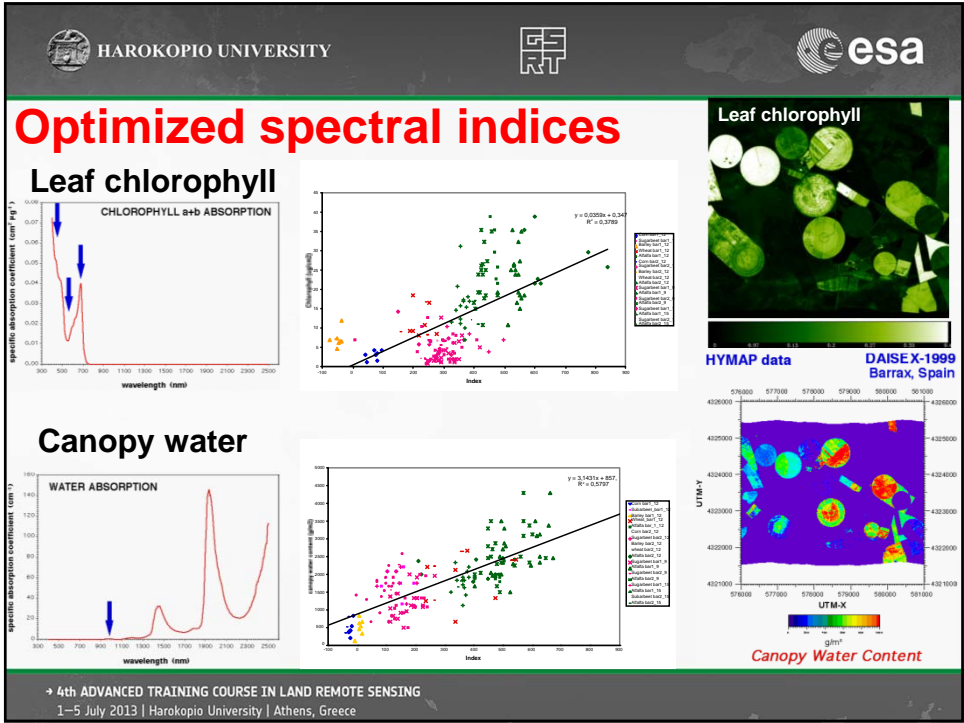




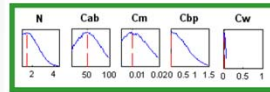
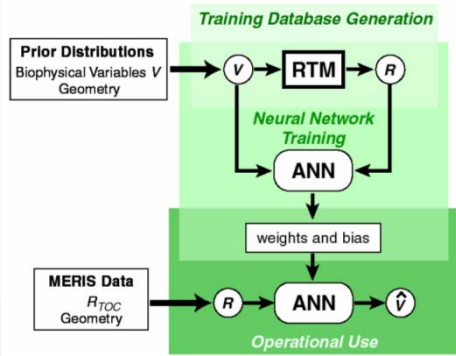
MERIS Terrestrial Chlorophyll Index (MTCI)

$$MTCI = \frac{R_{Band10} - R_{Band9}}{R_{Band9} - R_{Band8}}$$

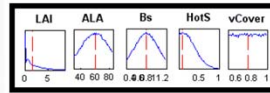




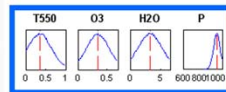
Neural network methods



Leaves

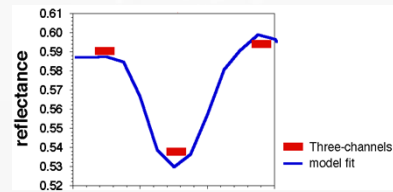
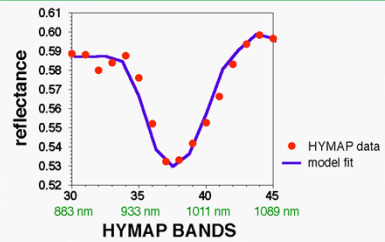
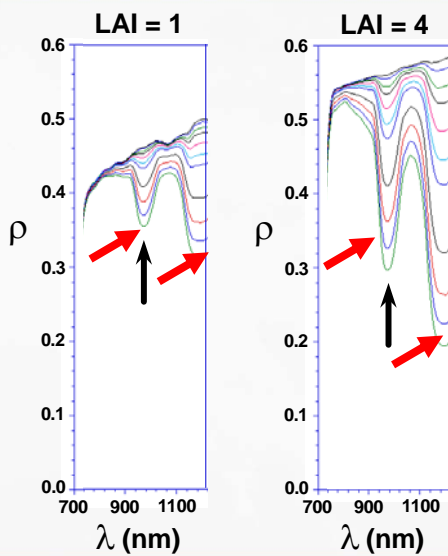


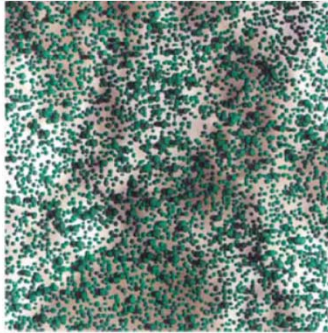
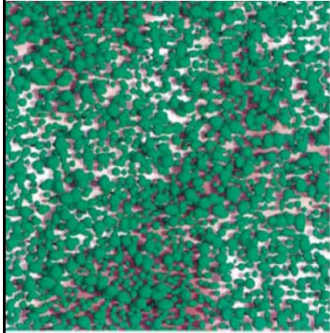
Canopy



Atmosphere

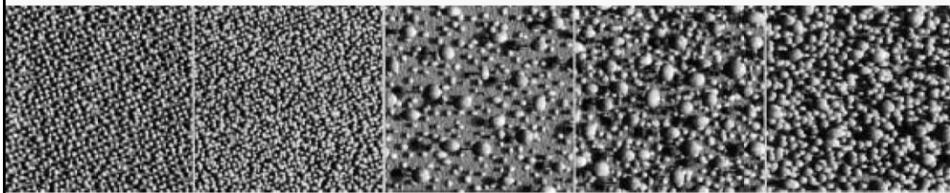
Training becomes the critical issue





Spatial information in the images

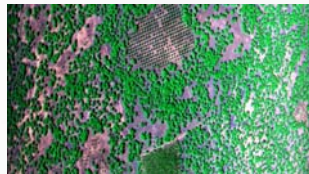
- Textures
- Higher order statistics



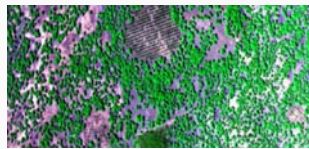
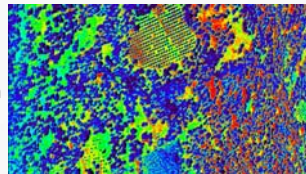
Multiresolution data

VIS/NIR/SWIR Colour Composite

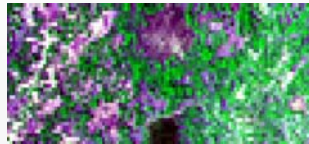
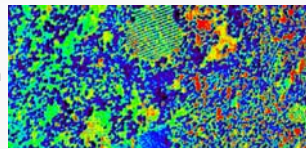
Thermal data



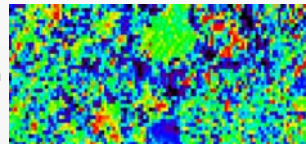
1.25 m

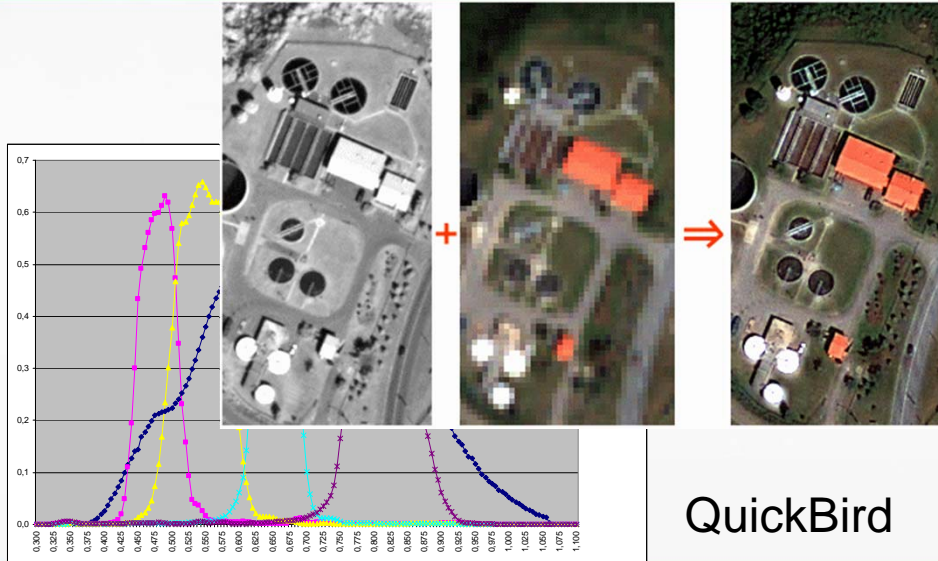


3.75 m

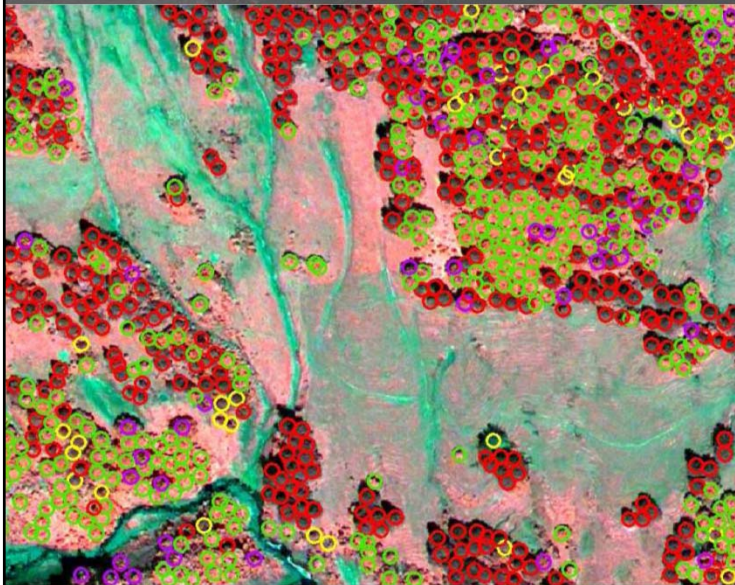


12.0 m

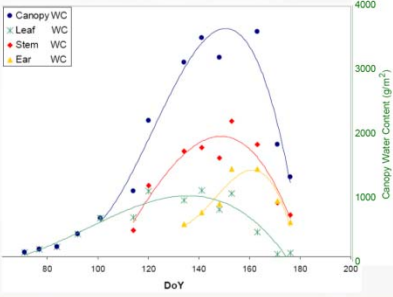
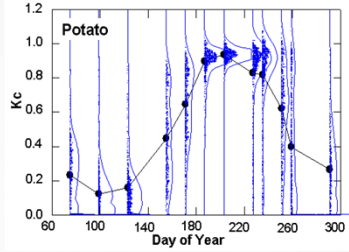




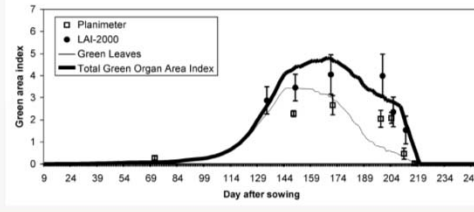
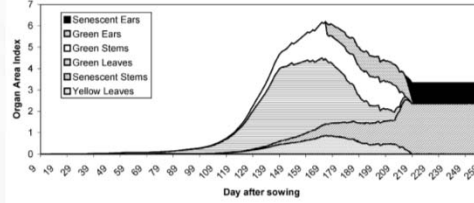
QuickBird



counting individual trees by using Quickbird very high resolution imagery



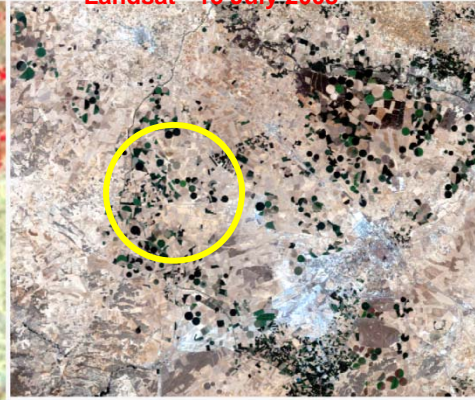
Time series: Coupling canopy functioning and radiative transfer models for remote sensing data assimilation



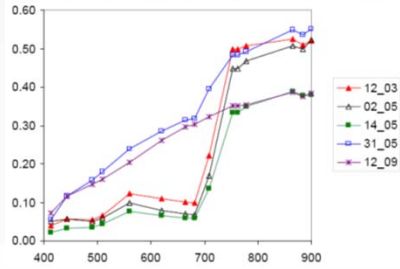
MERIS - 14 July 2003



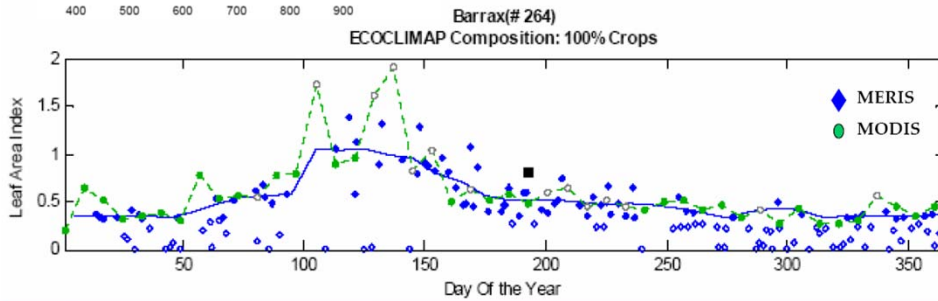
Landsat - 15 July 2003



MERIS and Landsat both provide time series at different spatial and temporal scales



**Stable calibration,
adequate cloud screening
and precise atmospheric
corrections are needed for
time series analysis**



ISSUES ABOUT VALIDATION OF RETRIEVALS

- Statistical representativity of measurements used for validation
- Strategy for spatial and temporal sampling
- Validation methodology versus retrieval technique
- Statistical extrapolation of results (sample versus population)
- Adaptation of different methodology for each biophysical parameter
- Examination of results in view of the expected limitations
- Adaptability to the application
- Critical review of actual achievements



Usage of the derived information:

- Tendency: from proxies to quantitative information
- Multi-resolution spatial inputs and time series

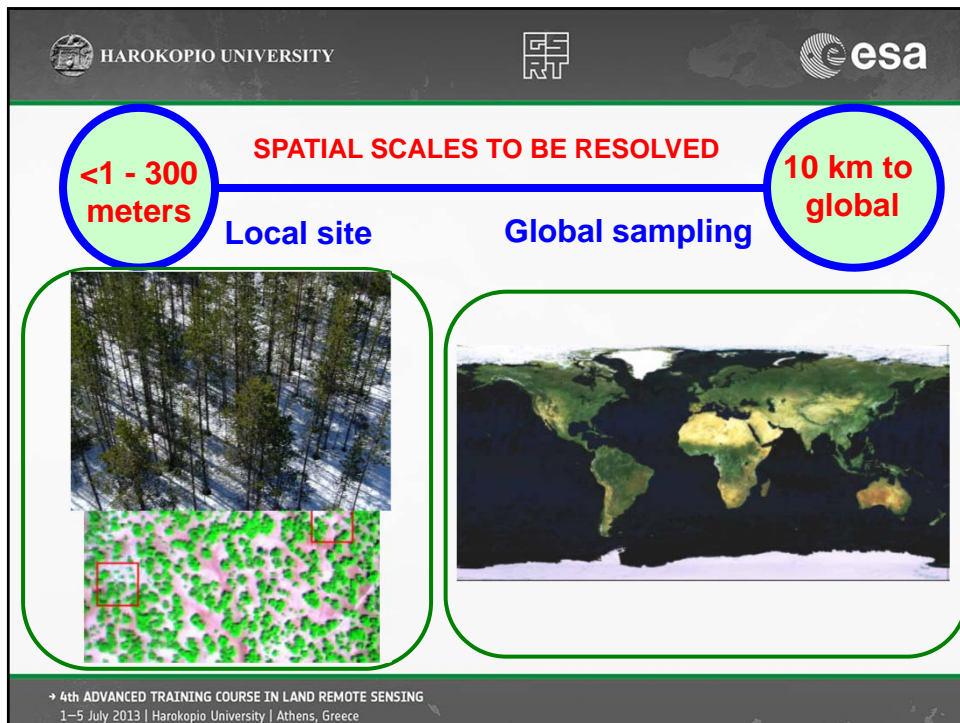
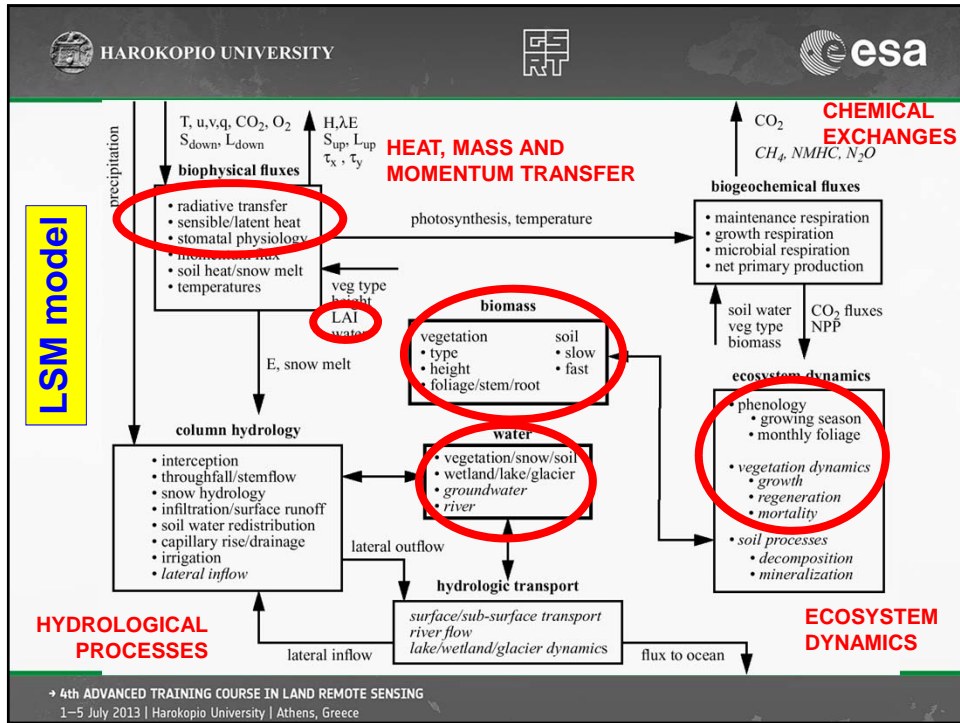
- **First approach:** Land cover mapping, classification and tables of biophysical variables assigned to each class
- **Second approach:** Retrievals of biophysical variables as direct inputs to models
- **Third approach:** direct assimilation of radiances/reflectances into models



REMOTE SENSING OF LAND SURFACE PROCESSES

- **Mapping Applications**
 - cartography
 - thematic mapping
- **Monitoring Applications**
 - ecosystems dynamics
 - natural hazards (fires, floods, desertification)
- **Research about Land Surface Processes**
 - heat and mass exchange at Land/Atmosphere interface
 - photosynthesis and net primary production
 - hydrologic processes
 - Land/Atmosphere exchange of biochemicals







3 - 10 days

TIME SCALES TO BE RESOLVED

> 3 years

Process modelled	Extent to which vegetation acts as a dynamic component	Timescale at which processes are modelled
<ul style="list-style-type: none"> Photosynthesis and leaf respiration. 	Stomata responds to variability in environmental conditions and CO ₂ concentration when coupling between photosynthesis and stomatal conductance is explicitly modelled.	Minutes to months
<ul style="list-style-type: none"> Growth respiration and stem and root maintenance respiration. 	Estimating respiration allows us to model NPP. $GPP - R_g = NPP$.	Minutes to months
<ul style="list-style-type: none"> Allocation 	Biomass allocated to leaves determines LAI. LAI thus varies with change in climatic conditions from year to year, and the seasonal cycle of LAI can be simulated rather than being prescribed.	Daily to annual
<ul style="list-style-type: none"> Phenology 	The timing of leaf onset and offset is modeled rather than be prescribed.	Daily to monthly
<ul style="list-style-type: none"> Nitrogen cycle 	Explicitly modeling N cycle and plant N uptake implies that N availability does not have to be assumed constant. The effect of variability in N availability on plant productivity can thus be modeled.	Monthly to annual
<ul style="list-style-type: none"> Competition between plant functional types (PFTs). 	Vegetation reacts to long-term changes in climate, and PFTs, which are best suited for a given region and climate, succeed.	Decades to centuries

Requires very large time series



EO Applications

- Calibration & Validation
- Vegetation monitoring
- Agriculture
- Forestry
- Water quality
- Climate change
- Damage Assessment
- Cartography

Methods

- Physical models
- Instrument design
- Image processing and analysis
- Automatic classification
- Analysis of time series
- Biophysical parameter estimation
- Data fusion



NEW GENERATION OF SENSORS

- Well calibrated (more suitable for multitemporal studies)
- Increased spatial resolution (0.5 m PAN now available)
- Increased spatial coverage (global mapping in high spatial resolution (as ESA GMES/Sentinel-2))
- New type of information (i.e., vegetation fluorescence)
- Time series: gap filling using multi-sensor data, better temporal resolution with high spatial resolution
- Integration of multi-resolution data with diverse spectral information in common temporal databases



The near future



GMES / Sentinels